



PRODUCT REPORT[®]

FraserWood Structural Glued Laminated Timber FraserWood Industries Ltd.

PR-L355

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Products: FraserWood Structural Glued Laminated Timber
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1. Basis of the product report:
 - 2024, 2021, 2018, and 2015 International Building Code (IBC): Section 2303.1.3 Structural glued laminated timber
 - 2024, 2021, 2018, and 2015 International Residential Code (IRC): Sections R502.1.3, R602.1.3, and R802.1.2 Structural glued laminated timber
 - ANSI 117-2020 and ANSI 117-2015 recognized in the 2024 and 2021 IBC and IRC, and 2018 IBC and IRC, respectively
 - ANSI A190.1-2022, ANSI A190.1-2017, and ANSI A190.1-2012 recognized in the 2024 IBC and IRC, 2021 and 2018 IBC and IRC, and 2015 IBC and IRC, respectively
 - 2024, 2018, and 2015 ANSI/AWC NDS, National Design Specification for Wood Construction recognized in the 2024 IBC and IRC, 2021 and 2018 IBC and IRC, and 2015 IBC and IRC, respectively
 - ASTM D3737-18e1 and D3737-12 recognized in the 2024 and 2021 IBC and IRC, and 2018 and 2015 IBC and IRC, respectively
 - Qualification test data
2. Product description:

FraserWood glulam products are manufactured with Alaska cedar, Douglas fir-Larch, and Port Orford cedar in accordance with ANSI A190.1. These layup combinations are recognized in ANSI 117. FraserWood glulam products are used as beams, headers, rafters, purlins, and columns, and are manufactured in nominal widths up to 15-3/4 inches, depths up to 36 inches, and lengths up to 60 feet.
3. Design properties:

Allowable design properties for FraserWood glulam beams and columns are listed in Tables 1 and 2. The allowable spans for FraserWood glulam beams shall be in accordance with the recommendations provided by the manufacturer and APA Data File: *Glued Laminated Beam Design Tables*, Form S475 (www.apawood.org/resource-library), as applicable, or shall be determined based on the design properties listed in Table 1, as appropriate. The allowable loads for FraserWood glulam columns shall be in accordance with the recommendations provided by the manufacturer and APA Data File: *Design of Structural Glued Laminated Timber Columns*, Form Y240 (see link above), as applicable, or shall be determined based on the design properties listed in Table 2, as appropriate.
4. Product installation:

FraserWood glulam beams and columns shall be installed in accordance with the recommendations provided by the manufacturer and APA Construction Guide: *Glulam Connection Details*, Form T300 (see link above). Permissible field notching and drilling of FraserWood glulam beams shall be in accordance with the recommendations provided by the manufacturer and APA Technical Notes: *Field Notching and Drilling of Glued Laminated Timber Beams*, Form S560, and *Effect of Large Diameter Horizontal Holes on the Bending and Shear Properties of Structural Glued Laminated Timber*, Form V700 (see link above).

Permissible field notching and drilling of FraserWood glulam columns shall be in accordance with the recommendations provided by the manufacturer.

5. Fire-rated assemblies:
Design of fire-resistant exposed wood members in accordance with Chapter 16 of the National Design Specification for Wood Construction (NDS) or Section 722.1 of the 2024, 2021, 2018, and 2015 IBC shall be applicable to FraserWood glulam products. Fire-rated assemblies shall be constructed in accordance with the recommendations provided by the manufacturer and APA Design and Construction Guide: *Fire-Rated Systems*, Form W305 (see link above).
6. Limitations:
 - a) FraserWood glulam beams and columns listed in this report shall be designed in accordance with the applicable code and the National Design Specification for Wood Construction using the allowable design properties specified in this report.
 - b) FraserWood glulam beams and columns shall meet the dimensions specified in ANSI 117 and ANSI A190.1.
 - c) FraserWood glulam beams and columns listed in this report are produced at the FraserWood Industries Ltd., Squamish, British Columbia facility under a quality assurance program audited by APA.
 - d) This report is subject to re-examination in one year.
7. Identification:
FraserWood glulam beams and columns described in this report are identified by a label bearing the manufacturer's name (FraserWood) and/or trademark, the APA assigned plant number (1111), the product standard (ANSI A190.1), the APA logo, the layup combination symbol, the report number PR-L355, and a means of identifying the date of manufacture.

Table 1. Allowable Design Values for FraserWood Glulam Beams for Normal Duration of Load^(1,2,3)

Symbol	Species Outer/ Core ⁽⁴⁾ (Bal or Unbal ⁽⁵⁾)	Bending About X-X Axis (Loaded Perpendicular to Wide Faces of Laminations)								Bending About Y-Y Axis (Loaded Parallel to Wide Faces of Laminations)						Axially Loaded		Fasteners	
		Extreme Fiber in Bending ⁽⁶⁾		Compression Perpendicular to Grain		Shear Parallel to Grain ⁽⁷⁾	Modulus of Elasticity ⁽⁸⁾			Extreme Fiber in Bending ⁽⁹⁾	Comp. Perpen-dicular to Grain	Shear Parallel to Grain ⁽⁷⁾	Modulus of Elasticity ⁽⁸⁾			Tension Parallel to Grain	Comp. Parallel to Grain	Specific Gravity for Dowel-Type Fastener Design	
		Bottom of Beam Stressed in Tension (Positive Bending)	Top of Beam Stressed in Tension (Negative Bending)	Ten. Face	Comp. Face		True	App-arent	Beam Stabi-lity				True	App-arent	Beam Stabi-lity			Top or Bottom Face	Side Face
		F _{bx} ⁺ (psi)	F _{bx} ⁻ (psi)	F _{cLx} (psi)		F _{vx} (psi)	E _{x true} (10 ⁶ psi)	E _{x app} (10 ⁶ psi)	E _{x min} (10 ⁶ psi)	F _{by} (psi)	F _{cLy} (psi)	F _{vy} (psi)	E _{y true} (10 ⁶ psi)	E _{y app} (10 ⁶ psi)	E _{y min} (10 ⁶ psi)	F _t (psi)	F _c (psi)	SG	
20F-V12	AC/AC (U)	2,000	1,400	560	560	265	1.6	1.5	0.79	1,250	470	230	1.5	1.4	0.74	925	1,500	0.46	0.46
20F-V13	AC/AC (B)	2,000	2,000	560	560	265	1.6	1.5	0.79	1,250	470	230	1.5	1.4	0.74	950	1,550	0.46	0.46
20F-V14	POC/POC (U)	2,000	1,450	560	560	265	1.6	1.5	0.79	1,300	470	230	1.5	1.4	0.74	900	1,600	0.46	0.46
20F-V15	POC/POC (B)	2,000	2,000	560	560	265	1.6	1.5	0.79	1,300	470	230	1.5	1.4	0.74	900	1,600	0.46	0.46
24F-V4	DF/DF (U)	2,400	1,850	650	650	265	1.9	1.8	0.95	1,450	560	230	1.7	1.6	0.85	1,100	1,650	0.50	0.50
24F-V8	DF/DF (B)	2,400	2,400	650	650	265	1.9	1.8	0.95	1,550	560	230	1.7	1.6	0.85	1,100	1,650	0.50	0.50
Wet-use factor		0.8		0.53		0.875	0.833			0.8	0.53	0.875	0.833			0.8	0.73	see NDS	

- ⁽¹⁾ The combinations in this table are applicable to members consisting of 4 or more laminations and are intended primarily for members stressed in bending due to loads applied perpendicular to the wide faces of the laminations. Allowable design values are tabulated, however, for loading both perpendicular and parallel to the wide faces of the laminations.
- ⁽²⁾ The tabulated allowable design values are for normal duration of loading. For other durations of loading, see the applicable building code. The tabulated allowable design values are for dry conditions of use. For wet conditions of use, multiply the tabulated values by the wet-use factors shown at the bottom of the table.
- ⁽³⁾ Referenced design values must be adjusted, as applicable, in accordance with Section 5.3 of the NDS.
- ⁽⁴⁾ AC = Alaska cedar, DF = Douglas fir-Larch, and POC = Port Orford cedar.
- ⁽⁵⁾ The unbalanced (U) layout is intended primarily for simple-span applications and the balanced (B) layout is intended primarily for continuous or cantilevered applications.
- ⁽⁶⁾ The values of F_{bx} are based on members 5-1/8 inches in width by 12 inches in depth by 21 feet in length. For members with a larger volume, F_{bx} shall be multiplied by a volume factor, C_v = (5.125/b)^{1/10} (12/d)^{1/10} (21/L)^{1/10}, where b is the beam width (in.), d is the beam depth (in.), and L is the beam length between the points of zero moment (ft).
- ⁽⁷⁾ For non-prismatic members, members subject to impact or cyclic loading, or shear design of bending members at connections (2024 NDS 3.4.4.1 or 2018 and 2015 NDS 3.4.3.3), the F_{vx} and F_{vy} values shall be multiplied by a factor of 0.72. The tabulated F_{vy} values are for timbers with laminations made from a single piece of lumber across the width or multiple pieces that have been edge bonded. For timber manufactured from multiple piece laminations (across width) that are not edge bonded, value shall be multiplied by 0.4 for members with 5, 7, or 9 laminations or by 0.5 for all other members.
- ⁽⁸⁾ The tabulated E values include true E (also known as "shear-free E"), apparent E, and E for beam stability calculation (NDS 3.3.3.8). For calculating beam deflections, the tabulated E_{app} values shall be used unless the shear deflection is determined in addition to bending deflection based on the tabulated E_{true}. The axial modulus of elasticity, E_{axial} and E_{axial min}, shall be equal to the tabulated E_{y true} and E_{y min} values.
- ⁽⁹⁾ The values of F_{by} are based on members 12 inches in depth. For depths less than 12 inches, F_{by} shall be permitted to be increased by multiplying by the flat use factor, (12/d)^{1/9}, where d is the beam depth in inches. When d is less than 3 inches, use the size adjustment factor for 3 inches.

Table 2. Allowable Design Values for FraserWood Glulam Columns for Normal Duration of Load^(1,2)

Combination Symbol	Species ⁽³⁾	Grade	All Loading				Axially Loaded			Bending about Y-Y Axis				Bending about X-X Axis		Fasteners Specific Gravity for Dowel-Type Fastener Design
			Modulus of Elasticity ⁽⁴⁾			Compression Perpendicular to Grain	Tension Parallel to Grain	Compression Parallel to Grain		Loaded Parallel to Wide Faces of Laminations			Shear Parallel to Grain ^(6,7)	Loaded Perpendicular to Wide Faces of Laminations		
							2 or More Lams	4 or More Lams	2 or 3 Lams	Bending ⁽⁵⁾				Bending ⁽⁸⁾ 2 Lams to 15 in. Deep ⁽⁹⁾	Shear Parallel to Grain ⁽⁶⁾	
			$E_{x \text{ true}}, E_{y \text{ true}}$ or E_{axial} (10 ⁶ psi)	$E_{x \text{ app}}$ or $E_{y \text{ app}}$ (10 ⁶ psi)	$E_{x \text{ min}}, E_{y \text{ min}}$ or $E_{\text{axial min}}$ (10 ⁶ psi)	$F_{c\perp}$ (psi)	F_t (psi)	F_c (psi)	F_c (psi)	F_{by} (psi)	F_{by} (psi)	F_{by} (psi)	F_{vy} (psi)	F_{bx} (psi)	F_{vx} (psi)	SG
1	DF	L3	1.6	1.5	0.79	560	950	1,550	1,250	1,450	1,250	1,000	230	1,250	265	0.50
2	DF	L2	1.7	1.6	0.85	560	1,250	1,950	1,600	1,800	1,600	1,300	230	1,700	265	0.50
3	DF	L2D	2.0	1.9	1.00	650	1,450	2,300	1,900	2,100	1,850	1,550	230	2,000	265	0.50
4	DF	L1CL	2.0	1.9	1.00	590	1,400	2,100	1,950	2,200	2,000	1,650	230	2,100	265	0.50
5	DF	L1	2.1	2.0	1.06	650	1,650	2,400	2,100	2,400	2,100	1,800	230	2,200	265	0.50
69	AC	L3	1.3	1.2	0.63	470	725	1,150	1,100	1,100	975	775	230	1,000	265	0.46
70	AC	L2	1.4	1.3	0.69	470	975	1,450	1,450	1,400	1,250	1,000	230	1,350	265	0.46
71	AC	L1D	1.7	1.6	0.85	560	1,250	1,900	1,900	1,850	1,650	1,400	230	1,750	265	0.46
72	AC	L1S	1.7	1.6	0.85	560	1,250	1,900	1,900	1,850	1,650	1,400	230	1,900	265	0.46
73	POC	L3	1.4	1.3	0.69	470	775	1,500	1,200	1,200	1,050	825	230	1,050	265	0.46
74	POC	L2	1.5	1.4	0.74	470	1,050	1,900	1,550	1,450	1,300	1,100	230	1,400	265	0.46
75	POC	L1D	1.8	1.7	0.90	560	1,350	2,300	2,050	1,950	1,750	1,500	230	1,850	265	0.46
Wet-use factors			0.833			0.53	0.8	0.73		0.8			0.875	0.8	0.875	see NDS

⁽¹⁾ The tabulated allowable design values are for normal duration of loading. For other durations of loading, see applicable building code. The tabulated allowable design values are for dry conditions of use. For wet conditions of use, multiply the tabulated values by the factors shown at the bottom of the table.

⁽²⁾ Referenced design values must be adjusted, as applicable, in accordance with Section 5.3 of the NDS.

⁽³⁾ AC = Alaska cedar, DF = Douglas fir-Larch, and POC = Port Orford cedar.

⁽⁴⁾ The tabulated E values include shear-free (true) modulus of elasticity ($E_{x \text{ true}}$, $E_{y \text{ true}}$, and E_{axial}), apparent modulus of elasticity ($E_{x \text{ app}}$ and $E_{y \text{ app}}$), and 5th percentile modulus of elasticity ($E_{x \text{ min}}$, $E_{y \text{ min}}$, and $E_{\text{axial min}}$). For column stability calculation (NDS 3.7.1), $E_{\text{axial min}}$ shall be used. For calculating the total deflection due to bending, the tabulated $E_{x \text{ app}}$ or $E_{y \text{ app}}$ values shall be used, or as an alternative, the true (shear-free) bending deflection shall be calculated using the tabulated $E_{x \text{ true}}$ or $E_{y \text{ true}}$, which shall be added to the calculated shear deflection to determine the total deflection due to bending.

⁽⁵⁾ The values of F_{by} are based on members 12 inches in depth. For depths less than 12 inches, F_{by} shall be permitted to be increased by multiplying by the flat use factor, $(12/d)^{1/9}$, where d is the beam depth in inches. When d is less than 3 inches, use the size adjustment factor for 3 inches.

⁽⁶⁾ For non-prismatic members, notched members, members subject to impact or cyclic loading, or shear design of bending members at connections (2024 NDS 3.4.4.1 or 2018 and 2015 NDS 3.4.3.3), the tabulated F_{vx} and F_{vy} values shall be multiplied by 0.72.

⁽⁷⁾ The tabulated F_{vy} values are for members of 4 or more lams. The tabulated F_{vy} values shall be multiplied by a factor of 0.95 for 3 lams and 0.84 for 2 lams. For members with 5, 7, or 9 lams manufactured from multiple-piece lams with unbonded edge joints, the tabulated F_{vy} values shall be multiplied by a factor of 0.4. For all other members manufactured from multiple-piece lams with unbonded edge joints, the tabulated F_{vy} values shall be multiplied by a factor of 0.5. This adjustment shall be cumulative with the adjustment specified in Footnote 6.

⁽⁸⁾ The values of F_{bx} are based on members 5-1/8 inches in width by 12 inches in depth by 21 feet in length. For members with a larger volume, F_{bx} shall be multiplied by a volume factor, $C_v = (5.125/b)^{1/10} (12/d)^{1/10} (21/L)^{1/10}$, where b is the beam width (in.), d is the beam depth (in.), and L is the beam length between the points of zero moment (ft).

⁽⁹⁾ The tabulated F_{bx} values are for members without special tension lams up to 15 inches in depth. If the member depth is greater than 15 inches without special tension lams, the tabulated F_{bx} values must be multiplied by a factor of 0.88. If special tension lams are used, the tabulated F_{bx} values are permitted to be increased by a factor of 1.18 regardless of the member depth provided that the increased F_{bx} value does not exceed 2,400 psi. This factor shall be cumulative with the volume factor, C_v , specified in Footnote 8.

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